

15TH International Workshop On Micropiles

DESIGN AND IN-CONSTRUCTION GEOLOGIC CHARACTERIZATION OF MICROPILES

TO SUPPORT A HISTORIC TRANSMISSION LINE UPGRADE IN THE STEEP TALUS AND
BASALT SLOPES OF THE COLUMBIA RIVER GORGE

presented by Brian J. Olson, C.E.G. | Crux Subsurface

Bonneville-Hood River 115kV Transmission Line



Bonneville Power Administration (BPA) – Transmission Line Micropile Foundations

- Phase 1: Verification Testing + 3 Foundations
- Phase 2: Remaining 24 Structure Foundations

Historic Background

- Originally constructed between 1939-1941
- Transmitted much needed electricity from the Bonneville Dam to Eastern Oregon
- The westernmost 22-mile segment (Bonneville to Hood River) proved to be most difficult
- State-of-the-art Modular H-Frames



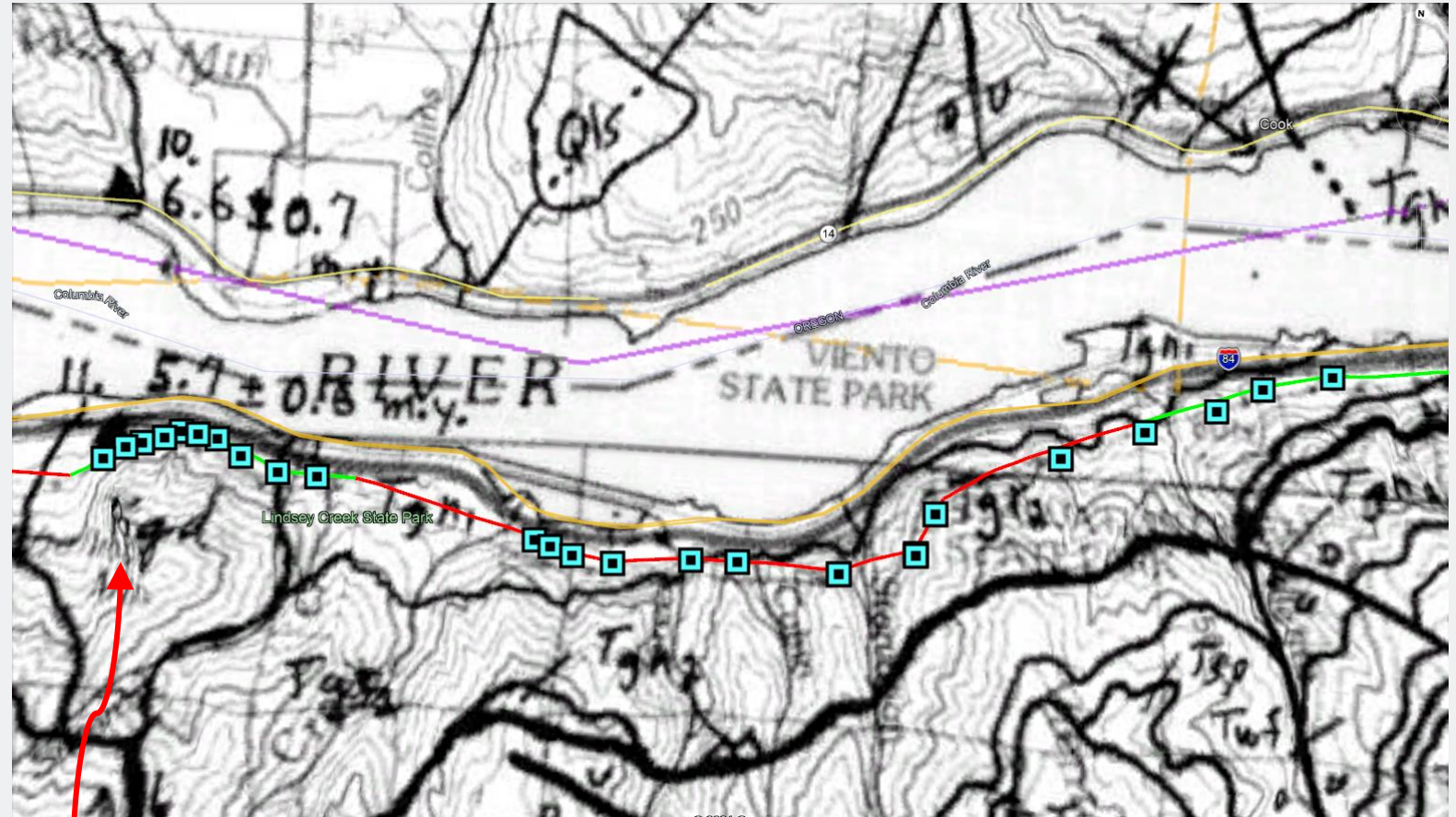
Historic Background

- Hand-excavated foundations supported the state-of-the-art modular H-Frame design
- Energized in 1941, it remained in service for over 75 years
- 68 structure sites along the segment
 - Drilled shafts designed for accessible sites
 - Micropiles at 26 locations with challenging access



Geologic Mapping - Bedrock

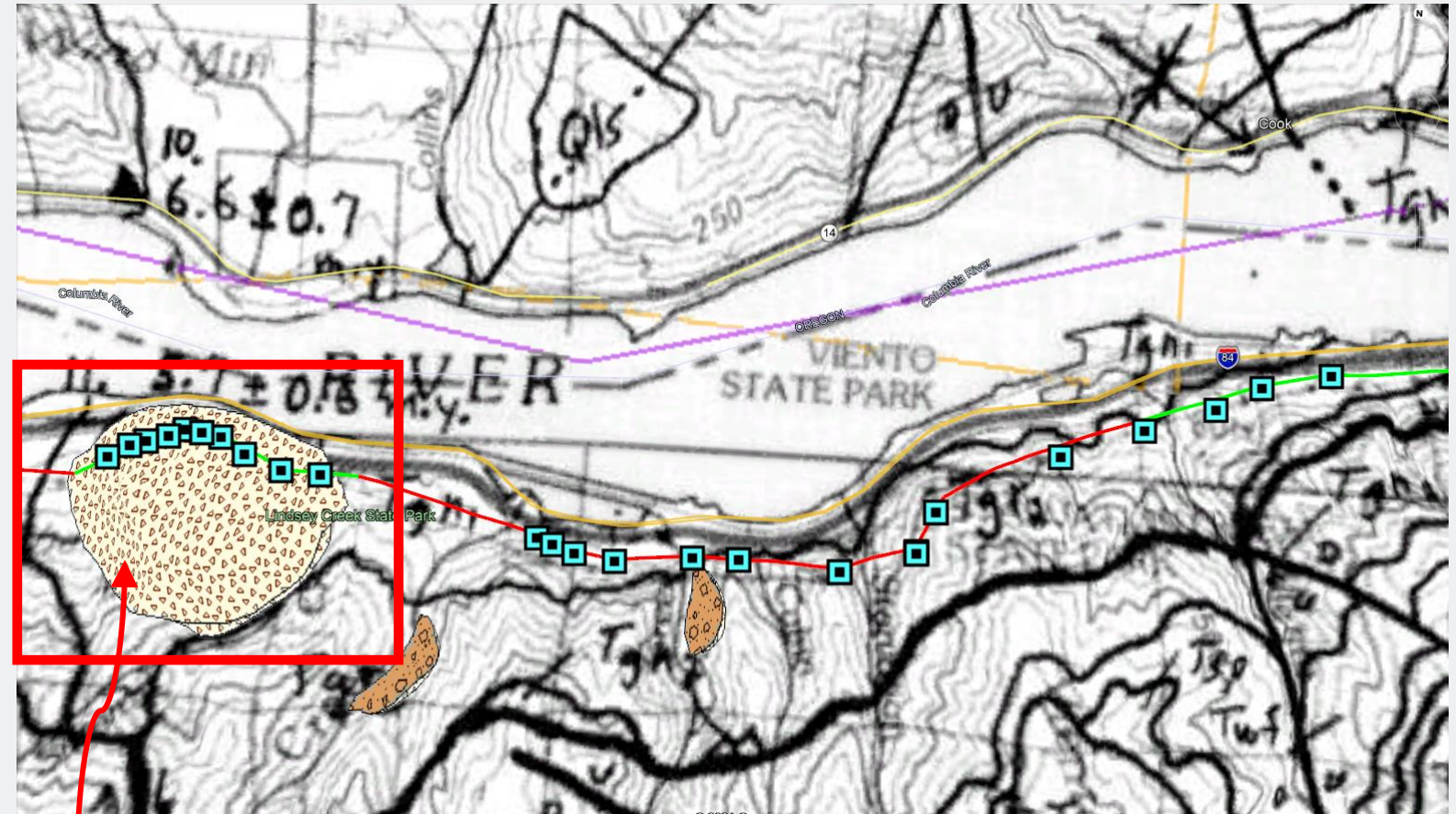
- Geologic Maps published by DOGAMI (Department of Geology and Mineral Industries)
- Kgd (Granodiorite) underlies Shell Rock
- Grand Ronde Basalt units to the east



SHELL ROCK

Geologic Mapping - Surficial Deposits

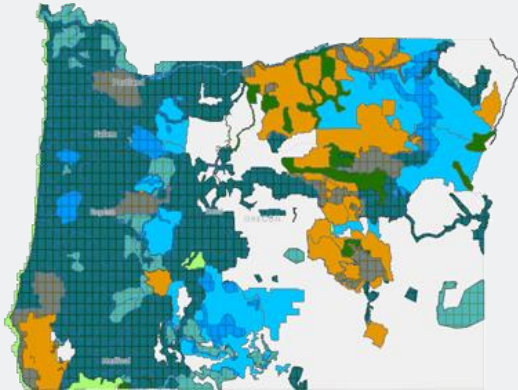
- Limited mapping of surficial deposits
- Existing landslide and talus mapping not well defined



SHELL ROCK

LiDAR and GIS

- Hillshade models derived from LiDAR
- Data maintained by DOGAMI



SHELL ROCK with LiDAR-Derived Hillshade

Bedrock Sites



- Grande Ronde Basalt of the Columbia River Basalt group
- Granitic rock would be encountered at depth in a lesser percentage of the foundations
- Micropile bond stress values for these bedrock types were well established
- Design parameters were relatively well defined
- Variations were limited to the depth and weathering profile of the bedrock
- Depth expected to vary considerably, sometimes across an individual tower footprint

Talus Sites



- Talus are an outward sloping and accumulated heap or mass of rock fragments of any size or shape (usually coarse and angular)
- Derived from, and laying at the base of, a cliff or very steep, rocky slope
- Here, consisted of angular gravel to boulder-sized basalt and granitic clasts shed from the elevated cliff areas south of the structure sites
- Although the interlocking angular deposits provide a high degree of global slope stability, the materials at the surface can be loosened when loaded by equipment or even heavy foot traffic.

Talus Sites - Challenges

- Bond stress values are not well established
- Clast size ranges from gravel to boulder
- Unit often masks underlying debris- or mud-flow deposits
- Voids within the larger clasts pose a challenge during drilling and grouting
- A verification test program to characterize this material was developed



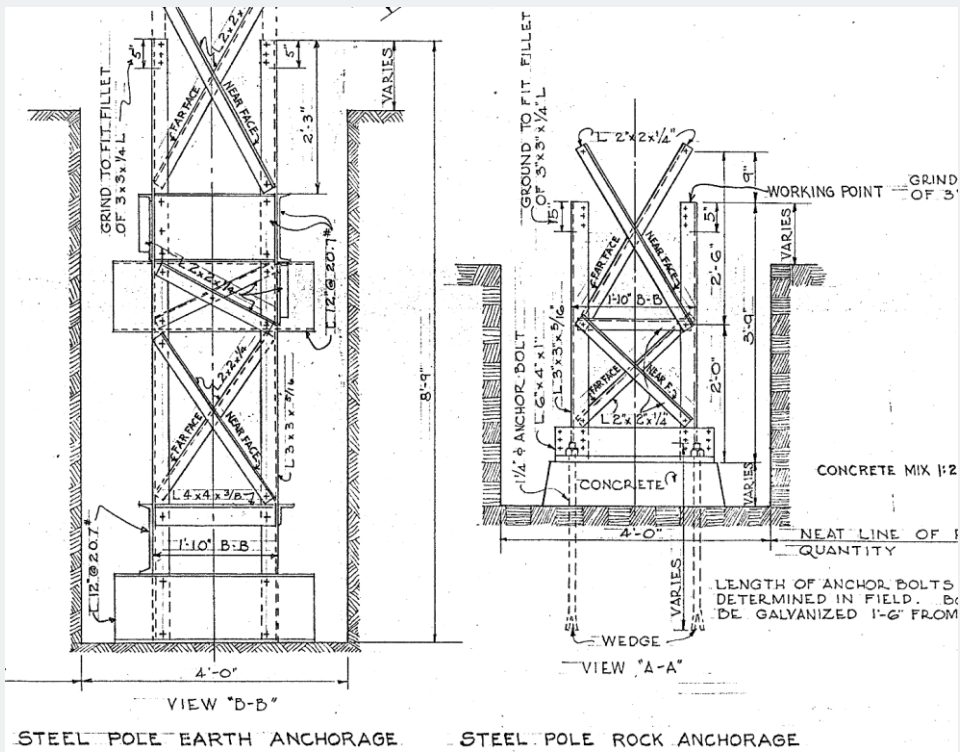
Soil Sites



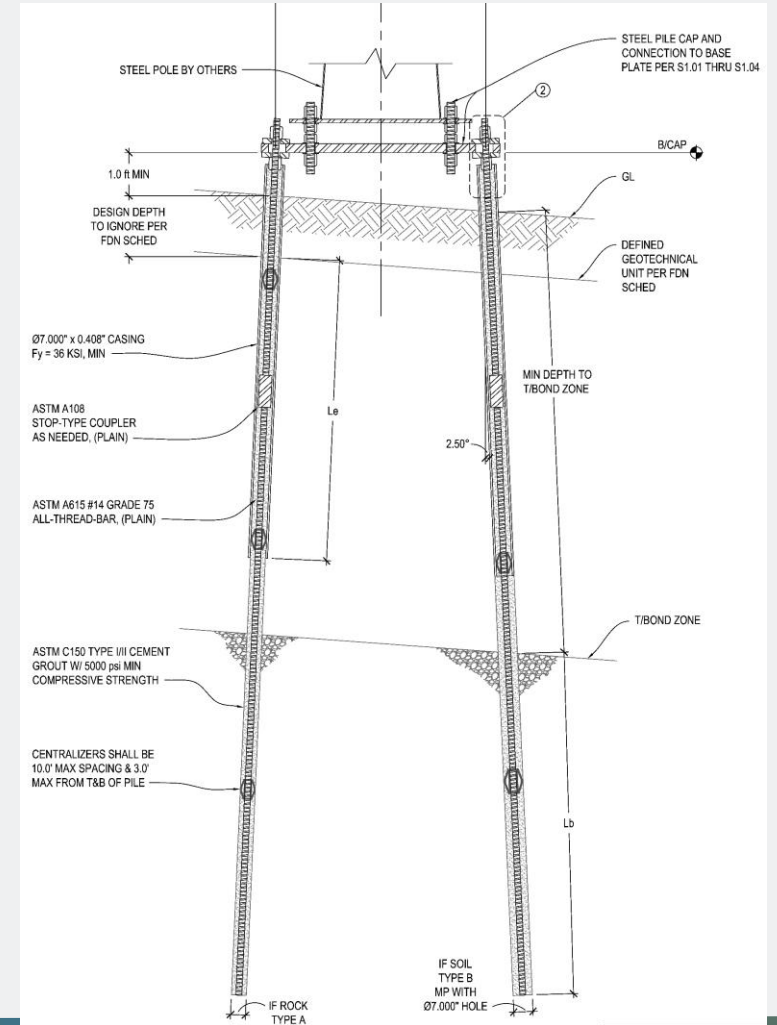
- Surficial talus deposits can hide buried finer grained soils and debris- or mud-flow deposits
- Contradicting bedrock outcrops or geologic mapping, deep soils would necessitate longer, specialized micropile bonds
 - Piles would need to be deepened to establish bonds in underlying bedrock
 - Or pressurized Type B or Type D bonds would be required
- Pre-construction desktop studies suggested soil deposits would be the least common category among the three

Before and After

1940



2018



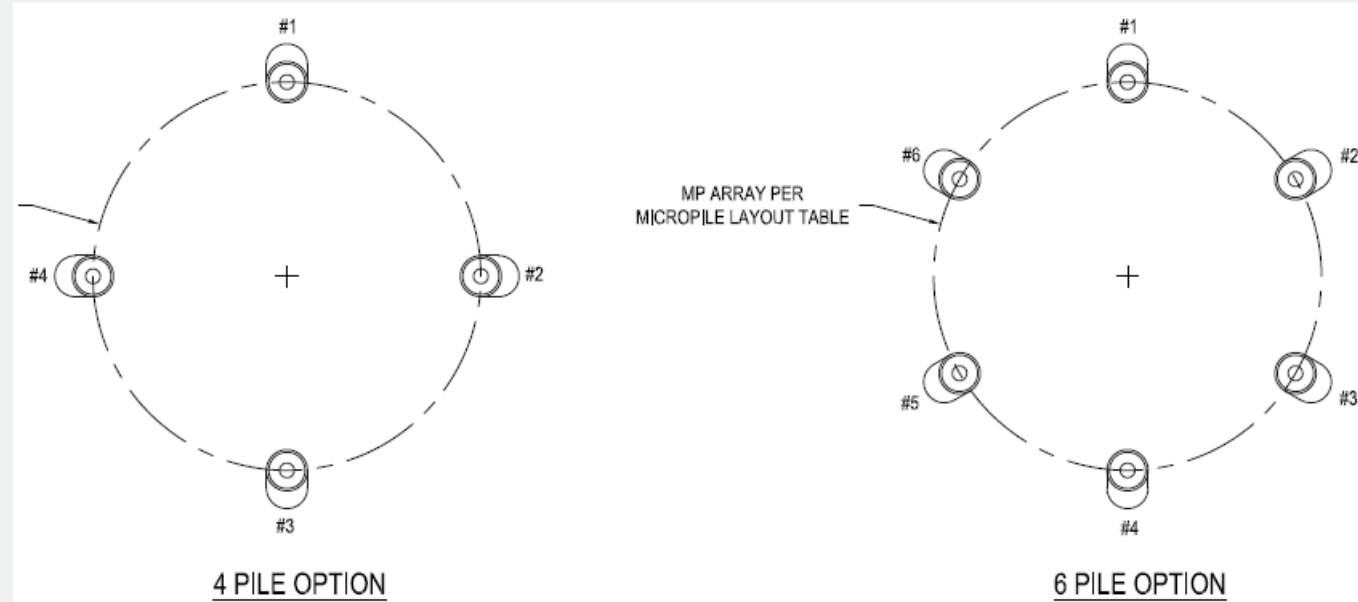
Foundation Design

- BPA Design Standards
 - Slope
 - Erosion/Scour
- Talus Characterization
 - Lateral Performance
 - Bond Stress
- Construction Tolerance
- Access Limits



Foundation Design

- Micropile Foundations
 - Portability
 - Steel pile caps
 - All helicopter equipment transport



| Maximum Foundation Design Loads | | | |
|---------------------------------|-------------|-------------|--------|
| | 4-Pile | 6-Pile | 8-Pile |
| Moment, (k-ft) | 907.1 | 1723.4 | 2142.1 |
| Axial, (k) | 15.3 | 83.8 | 12.8 |
| Shear, (k) | 13.8 | 29.5 | 14.2 |

Foundation Design

- Pile Arrays of 4, 6, and 8 Piles
 - Casing: 7" x 0.408"
 - Bar: #18 Gr 75, 2.25" 150ksi
 - Batter: 2.5 deg
 - Stick-up: 12" min at uphill side
 - Pinned vs Fixed
 - Corrosion Protection - Galvanized



Foundation Design



- Steel Pile Cap Design
 - FEA modeling for strength and performance
 - A572 Gr 50, Galvanized
 - Pile Cap Thickness:
 - Single Plate: 2.5"-4.5"
 - Double Plate: 5"-5.5"
 - Cap diameters ranged from 52-82"
 - Designed to serve as a reaction frame for load testing where possible

Foundation Design

- Foundation Schedule
 - Specific to each site
 - Allows flexibility in the field
 - Options based on varying soil/rock types, slopes, batter, pile materials
 - Each site characterized during drilling of first pile: cased zone and bond zone
 - QA/QC Requirements

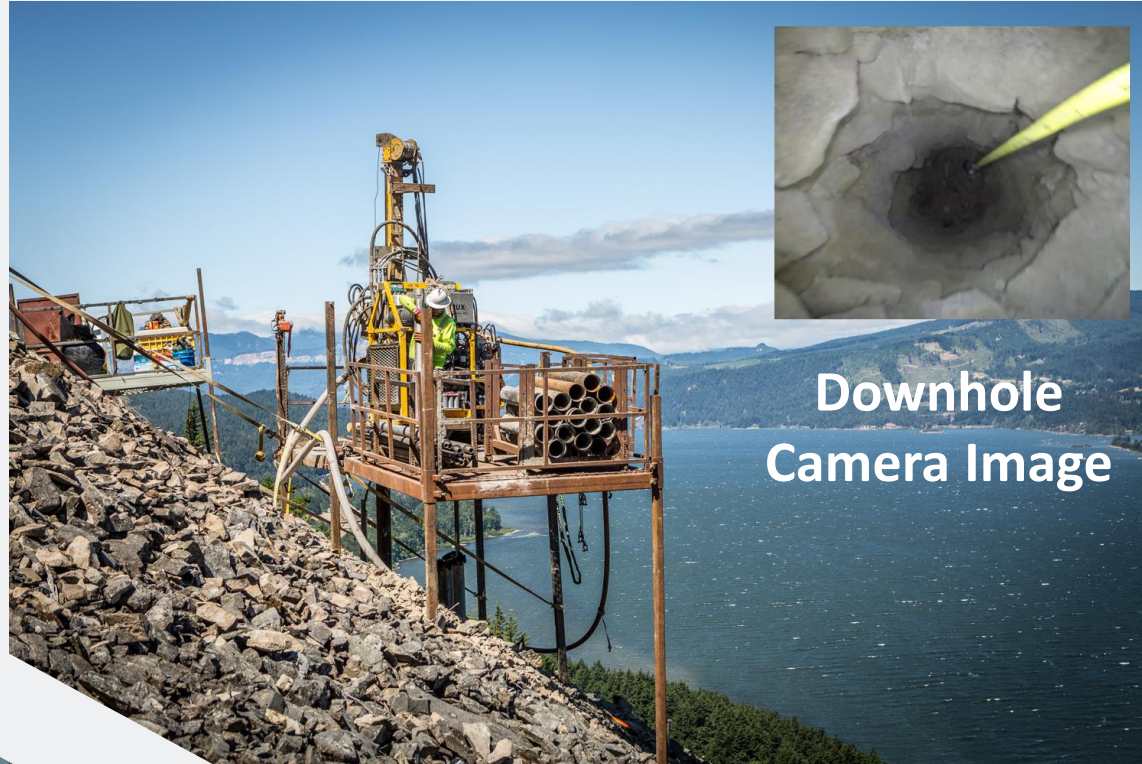
| Structure Number | Pile Config | Design Depth (ft) | Casing ID | Pile Size | Pile Material | Pile Length (ft) | No. of Piles | Casing Information (ft) | | | Bond Zone (ft) | | | | | Pile Test No. | Design Load (kips) | | | | | |
|------------------|-------------|-------------------|-----------|-----------|---------------|------------------|--------------|-------------------------|-------------|-----------------|----------------|------|------------------|-----------|--------------|---------------|--------------------|------------------|--------------------|------|-----|------|
| | | | | | | | | SPT Blows/ft | Soil | Case Depth (ft) | SPT Blows/ft | Soil | Pile Length (ft) | Pile Type | Insertion/ft | | | Test Load (kips) | Design Load (kips) | | | |
| 108 | CL-402 | 3 | 7 | 8x8 | 24 | 48 | 4 | 14 | Cased | 14.1 | 14.1 | 81 | 15-21 | CL-4 | B | 10.0 | 112 | 110.0 | | | | |
| | | | | | | | | | | | | | 21-27 | CL-4 | B | 10.0 | | | | | | |
| | | | | | | | | | | | | | 27-33 | CL-4 | B | 10.0 | | | | | | |
| | | | | | | | | | | | | | 33-39 | CL-4 | B | 10.0 | | | | | | |
| | | | | | | | | 1501 | Welded Case | 14.1 | 17.1 | 72 | 15-21 | CL-4 | 1.0 | 81 | | | 15-21 | CL-4 | 1.0 | 10.0 |
| | | | | | | | | | | | | | | | | | | | 21-27 | CL-4 | 1.0 | 10.0 |
| | | | | | | | | | | | | | | | | | | | 27-33 | CL-4 | 1.0 | 10.0 |
| | | | | | | | | | | | | | | | | | | | 33-39 | CL-4 | 1.0 | 10.0 |
| | | | | | | | | 30 | Cased | 14.1 | 19.1 | 72 | 15-21 | CL-4 | 1.0 | 81 | | | 15-21 | CL-4 | 1.0 | 10.0 |
| | | | | | | | | | | | | | | | | | | | 21-27 | CL-4 | 1.0 | 10.0 |
| | | | | | | | | | | | | | | | | | | | 27-33 | CL-4 | 1.0 | 10.0 |
| | | | | | | | | | | | | | | | | | | | 33-39 | CL-4 | 1.0 | 10.0 |
| 40 (P) | Cased | 14.1 | 21.1 | 72 | 15-21 | CL-4 | 1.0 | 81 | 15-21 | CL-4 | 1.0 | 10.0 | | | | | | | | | | |
| | | | | | | | | | 21-27 | CL-4 | 1.0 | 10.0 | | | | | | | | | | |
| | | | | | | | | | 27-33 | CL-4 | 1.0 | 10.0 | | | | | | | | | | |
| | | | | | | | | | 33-39 | CL-4 | 1.0 | 10.0 | | | | | | | | | | |
| 50 (P) | Cased | 14.1 | 23.1 | 72 | 15-21 | CL-4 | 1.0 | 81 | 15-21 | CL-4 | 1.0 | 10.0 | | | | | | | | | | |
| | | | | | | | | | 21-27 | CL-4 | 1.0 | 10.0 | | | | | | | | | | |
| | | | | | | | | | 27-33 | CL-4 | 1.0 | 10.0 | | | | | | | | | | |
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Load Testing – Verification Testing (Phase 1)

- Pre-production verification test program as a first order of work under the construction contract.
- Two sacrificial micropiles were installed in locations established by the owner.
- To define the bond zone strength for talus materials.
- confirming the adequacy of the installation methods.
- SPT sampling, geologic logging, and downhole camera video were utilized to document the geotechnical conditions in each of these sacrificial piles



Geologic Characterization and Monitoring



Downhole
Camera Image

- Geologists representing the Foundation Engineer of Record (EOR) were onsite to work with the drillers, confirm the subsurface conditions, and assign cased zone and bond zone IDs.
- Standard Penetrometer Test (SPT) sampling was performed in general accordance with ASTM D1586.
- Classification in general accordance with ASTM D2488.
- Downhole camera system specially adapted for micropile diameters.

Production QC – Proof Testing (Phase 2)



- Conducted on a percentage of total production piles installed
 - Verifies consistency of the construction procedure
 - Confirms application of soil/rock strengths
- When a high degree of geologic uncertainty exists and geotechnical bond units may vary due to:
 - Variations inherent in the geologic unit
 - Distance between the sacrificial test locations
- Proof testing was performed on all foundations where talus or soil bonds were installed

Keys to Success

- Steel Cap Design
- Handling unforeseen variability in the Talus materials
 - Pre-construction verification testing
 - Differentiating between Talus and finer grained alluvial/colluvial sites
- Proof testing of production piles at all Talus and Alluvial sites



Project Completion

Energized in the Fall of 2020



Questions?

